AE 6311: Advanced Structural Dynamics Homework 4

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Problem 1

Problem Statement

For the 3-dof system with K, M, and F shown below, find the forcing frequency for $|U_2| = |U_3|$.

Solution

The method used to solve this problem is described in problem 2. The answer is

$$\Omega = 5.47723 \text{ rad/s} \tag{1}$$

Problem 2

Problem Statement

Develop a general method to solve the following problem: find the forcing frequency so that $|U_r(\Omega)| = a|U_s(\Omega)|$, where r and s are any two dof in the system, and a is a non-zero positive constant. The system is undamped with mass matrix **M**, stiffness matrix **K** and sinusoidal load amplitude vector **F**. Validate your solution by applying it to problem 1 and a 3-node beam model with load applied at the tip.

Solution

This type of problem can be solved using transfer functions. In general the equations of motion for a harmonically excited MDOF system can be written as

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{F}e^{i\Omega t} \tag{2}$$

Assuming a solution of the form

$$\mathbf{u}(t) = \mathbf{U}e^{i\Omega t} \tag{3}$$

and inserting it into (2),

$$\left(-\Omega^2 \mathbf{M} + i\Omega \mathbf{C} + \mathbf{K}\right) \mathbf{U} = \mathbf{F}$$
(4)

or

$$\mathbf{Z}\mathbf{U}=\mathbf{F}$$
(5)

where \mathbf{Z} is the impedance matrix. Now, the amplitudes of the steady-state responses can be solved for by

$$\mathbf{U} = \mathbf{Z}^{-1}\mathbf{F} \equiv \mathbf{H}\mathbf{F} \tag{6}$$

where H can be thought of as a matrix of transfer functions. Or,

$$U_i = \sum_{j=1}^N H_{ij} F_j \tag{7}$$

For one value,

$$|U_1| = |H_{11}F_1 + H_{12}F_2 + \ldots + H_{1N}F_N|$$
(8)

However, only one value of F is nonzero for the cases given. Letting the one nonzero value be m_r ,

$$|H_{rm}(\Omega)| = a|H_{sm}(\Omega)| \tag{9}$$

Now, the value of Ω can be determined by solving the polynomial in Ω given in (9). This approach is general and should work for any method that yields stiffness, mass and damping matrices.

For the problem in part A,

$$H_{21} = \frac{100. - 10.\Omega^2}{-1.\Omega^6 + 70.\Omega^4 - 1025.\Omega^2 + 2500.}$$
(10a)

$$H_{31} = -\frac{100.}{1.\Omega^6 - 70.\Omega^4 + 1025.\Omega^2 - 2500.}$$
(10b)

Solving for Ω yields

$$\Omega = 5.47723 \text{ rad/s} \tag{11}$$

For the 3-node beam model, the stiffness and mass matrices were determined using Ritz method.

For a beam with the following inputs,

The method yields

$$\Omega = 407622.99 \text{ rad/s}$$
 (12)

The equation to be solve was formed symbolically, then converted to a numeric function handle using matlabFunction. I then tried to use fzero, but sometimes got negative frequencies. Then, I

tried fminbnd and made sure that the solution was positive. A plot of the objective function seems to show multiple solutions. The solution found in this case is marked by the green dot.



Figure 1: Plot of the objective function that was used to solve for Ω in the beam problem.

Problem 3

Problem Statement

Compute and plot the frequency responses in 3 forms (Bode, Nyquist and CO-QUAD) for the beam of problem 4-2. Assume the system is proportionally damped. The modal damping ratios for the first two modes are 0.01. The applied load is a unit force at the tip. Plot the tip and midspan responses.

Solution

For proportional damping,

$$\mathbf{C} = a_0 \mathbf{M} + a_1 \mathbf{K}$$

Using this relation along with the other typical expressions from mode superposition, the modal damping ratio for the *r*-th mode can be related to the coefficients a_0 and a_1 .

$$\zeta_r = \frac{1}{2} \left(\frac{a_0}{\omega_r} + a_1 \omega_r \right)$$

Solving the system of equations for the constants yields

$$a_0 = \frac{2\omega_1 \omega_2 (\zeta_2 \omega_1 - \zeta_1 \omega_2)}{\omega_1^2 - \omega_2^2}$$
(13a)

$$a_1 = \frac{2\zeta_1 \omega_1 - 2\zeta_2 \omega_2}{\omega_1^2 - \omega_2^2}$$
(13b)

Because the loading is not harmonic, the typical approach for determining the frequency response functions won't work. Because of this, I used the Fast Fourier Transorm, which is an implementation of the discrete Fourier transform (DFT). The DFT of an N point signal, x[n] is

$$X[k] = \sum_{n=0}^{N-1} x[n] e^{-j2\pi kn/N}$$

A MATLAB function was written for taking the FFT and plotting the results. The frequency reponses of the tip and midspan translational responses are shown below.



Figure 2: Bode plot for tip.



Figure 4: Nyquist plot for tip.



Figure 5: Bode plot for midspan.



Figure 6: CO-QUAD plot for midspan.



Figure 7: Nyquist plot for midspan.

Problem 4

Problem Statement

Find the transient response of the system subject to a unit step force applied at the tip. Assume zero initial conditions.

Solution

This problem can be solved using Laplace transforms. I believe the system is undamped. The stiffness and mass matrices were formed using the Ritz method. The inputs to the code were:

L =	10;	%	in
E =	1e4;	%	psi
rho	= 0.1/386.4;	%	lb-s^2/in^4
A =	4;	%	in^2
I =	16/12;	%	in^4
N =	6;		

The system of ODEs can be written as

$$\sum_{j=1}^{N} M_{ij} \ddot{u}_j(t) + \sum_{j=1}^{N} K_{ij} u_j(t) = F_i(t)$$
(14)

Then, the index i is iterated over to form N differential equations. After doing so, the Laplace transform is applied to both sides. Assuming zero initial conditions,

$$\sum_{j=1}^{N} M_{ij} U_j(s) + \sum_{j=1}^{N} K_{ij} U_j(s) = \mathcal{L}[F_i]$$
(15)

The resulting algebraic system of equations is then solved for the U_j terms. Now, the inverse Laplace transform can be used to determine the responses as a function of time. This entire process was accomplished using Mathematica. The results are shown below.

Homework 4 Problem 4

In[156]:= ClearAll["Global`*"]

Inputs from MATLAB Ritz method code

$$\begin{split} \mbox{In[158]:= } M &= \{ \{ 0.001563, -0.000851, 0.000657, 0.001195 \}, \\ \{ -0.000851, 0.000598, -0.000657, -0.000896 \}, \{ 0.000657, -0.000657, \\ 0.004207, 0.000000 \}, \{ 0.001195, -0.000896, 0.000000, 0.009560 \} \}; \end{split}$$

```
ln[159]:= \mathbf{F} = \{1, 0, 0, 0\};
```

Forming the ODEs

```
In(160):= uvpp = {u1''[t], u2''[t], u3''[t], u4''[t]};
In(161):= uv = {u1[t], u2[t], u3[t], u4[t]};
In(162):= eqs = Table[Sum[M[[i]][[j]] uvpp[[j]], {j, 1, 4}] +
Sum[K[[i]][[j]] uv[[j]], {j, 1, 4}] == F[[i]], {i, 1, 4}]
Out[162]= {1939.81 u1[t] - 4335.24 u2[t] - 1365.33 u3[t] - 7314.29 u4[t] +
0.001563 u1"[t] - 0.000851 u2"[t] + 0.000657 u3"[t] + 0.001195 u4"[t] == 1,
-4335.24 u1[t] + 12647.6 u2[t] + 3413.33 u3[t] + 12190.5 u4[t] -
0.000851 u1"[t] + 0.000598 u2"[t] - 0.000657 u3"[t] - 0.000896 u4"[t] == 0,
0. - 1365.33 u1[t] + 3413.33 u2[t] + 2730.67 u3[t] + 0.000657 u1"[t] -
0.000657 u2"[t] + 0.004207 u3"[t] == 0, 0. - 7314.29 u1[t] + 12190.5 u2[t] +
48761.9 u4[t] + 0.001195 u1"[t] - 0.000896 u2"[t] + 0.00956 u4"[t] == 0}
```

```
In[163]:= Leqs = Table[LaplaceTransform[eqs[[i]], t, s], {i, 1, 4}]
Out[163]= {1939.81 LaplaceTransform[u1[t], t, s] - 4335.24 LaplaceTransform[u2[t], t, s] -
                           1365.33 LaplaceTransform[u3[t], t, s] - 7314.29 LaplaceTransform[u4[t], t, s] +
                           0.001563 (s<sup>2</sup> LaplaceTransform[u1[t], t, s] - su1[0] - u1'[0]) -
                           0.000851 (s<sup>2</sup> LaplaceTransform[u2[t], t, s] - su2[0] - u2'[0]) +
                           0.000657 (s^2 LaplaceTransform[u3[t], t, s] - su3[0] - u3'[0]) +
                          0.001195 (s<sup>2</sup> LaplaceTransform[u4[t], t, s] - su4[0] - u4'[0]) = \frac{1}{-1},
                    -4335.24 LaplaceTransform[u1[t], t, s] + 12647.6 LaplaceTransform[u2[t], t, s] +
                           3413.33 LaplaceTransform[u3[t], t, s] + 12190.5 LaplaceTransform[u4[t], t, s] -
                           0.000851 (s<sup>2</sup> LaplaceTransform[u1[t], t, s] - s u1[0] - u1'[0]) +
                           0.000598 (s<sup>2</sup> LaplaceTransform[u2[t], t, s] - su2[0] - u2'[0]) -
                           0.000657 (s<sup>2</sup> LaplaceTransform[u3[t], t, s] - su3[0] - u3'[0]) -
                           0.000896 (s<sup>2</sup> LaplaceTransform[u4[t], t, s] - su4[0] - u4'[0]) == 0,
                    0. - 1365.33 LaplaceTransform[u1[t], t, s] + 3413.33 LaplaceTransform[u2[t], t, s] +
                           2730.67 LaplaceTransform[u3[t], t, s] +
                           0.000657 (s^2 \text{ LaplaceTransform}[u1[t], t, s] - su1[0] - u1'[0]) -
                           0.000657 (s^2 \text{ LaplaceTransform}[u2[t], t, s] - su2[0] - u2'[0]) +
                           0.004207 (s^2 \text{ LaplaceTransform}[u3[t], t, s] - su3[0] - u3'[0]) = 0,
                    0. - 7314.29 LaplaceTransform[u1[t], t, s] + 12190.5 LaplaceTransform[u2[t], t, s] +
                           48761.9 LaplaceTransform[u4[t], t, s] +
                           0.001195 (s<sup>2</sup> LaplaceTransform[u1[t], t, s] - su1[0] - u1'[0]) -
                           0.000896 (s<sup>2</sup> LaplaceTransform[u2[t], t, s] - su2[0] - u2'[0]) +
                          0.00956 (s<sup>2</sup> LaplaceTransform[u4[t], t, s] - su4[0] - u4'[0]) = 0
 In[164]:= Ls = Solve[Leqs, Table[LaplaceTransform[uv[[i]], t, s], {i, 1, 4}]];
 In[165]:= ReplaceAll[Ls,
                       Thread[Rule[{u1[0], u1'[0], u2[0], u2'[0], u3[0], u3'[0], u4[0], u4'[0]},
                              \{0, 0, 0, 0, 0, 0, 0, 0, 0\}]];
 In[166]:= Lsf = Ls // Flatten;
 in(167):= soln = Table[InverseLaplaceTransform[Lsf[[i]], s, t], {i, 1, 4}];
 In[168]:= soln =
                       ReplaceAll[soln, Thread[Rule[{u1[0], u1'[0], u2[0], u2'[0], u3[0], u3'[0], u4[0],
                                       u4'[0]}, {0, 0, 0, 0, 0, 0, 0, 0}]]] // FullSimplify;
 In[169]:= resp1 = u1[t] /. soln[[1]]
Out[169] = 0.025 - 0.0121339 e^{(0.-126.173 i) t} - 0.0121339 e^{(0.+126.173 i) t} - 0.000313014 e^{(0.-794.983 i) t} - 0.0121339 e^{(0.+126.173 i) t} - 0.000313014 e^{(0.-794.983 i) t} - 0.0121339 e^{(0.-126.173 i) t} - 0.0121339 e^{(0.-126.173 i) t} - 0.0121339 e^{(0.-126.173 i) t} - 0.000313014 e^{(0.-794.983 i) t} - 0.0121339 e^{(0.-126.173 i) t} - 0.0121339 e^{(0.-126.173 i) t} - 0.000313014 e^{(0.-794.983 i) t} - 0.0121339 e^{(0.-126.173 i) t} - 0.000313014 e^{(0.-794.983 i) t} - 0.000314 e^{(0.-794.983 i) t} - 0.000314 e^{(0.-794.983 i) t} - 0.000312014 e^{(0.-
                    0.000313014 \ e^{(0.+794.983 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.+805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} - 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653 \ i) \ t} + 8.93183 \times 10^{-18} \ e^{(0.-805.653
                    0.0000440956 e^{(0.-2272.76 i) t} - 9.01835 \times 10^{-6} e^{(0.-10056.5 i) t} - 9.01835 \times 10^{-6} e^{(0.+10056.5 i) t}
```

ln[170]:= resp2 = u2[t] /. soln[[2]]

 $\begin{array}{l} \text{Out}[170]= & 0.00375 - 0.00167029 \ e^{(0.-126.173\ i)\ t} - 0.00167029 \ e^{(0.+126.173\ i)\ t} - \\ & 6.24539 \times 10^{-17} \ e^{(0.-553.858\ i)\ t} - 6.24539 \times 10^{-17} \ e^{(0.+553.858\ i)\ t} - 0.000149651 \ e^{(0.+794.983\ i)\ t} - \\ & 0.000149651 \ e^{(0.-794.983\ i)\ t} - 3.78529 \times 10^{-15} \ e^{(0.+805.653\ i)\ t} - 3.78529 \times 10^{-15} \ e^{(0.-805.653\ i)\ t} + \\ & 2.66053 \times 10^{-15} \ e^{(0.+1820.39\ i)\ t} + 2.66053 \times 10^{-15} \ e^{(0.-1820.39\ i)\ t} - \end{array}$

 $1.64967 \times 10^{-13} e^{(0.+2258.45 i) t} - 1.64967 \times 10^{-13} e^{(0.-2258.45 i) t} -$

 $0.0000346096 \; \mathrm{e}^{\,(0.+2272.76\,\mathrm{i})\;\mathrm{t}} - 0.0000346096 \; \mathrm{e}^{\,(0.-2272.76\,\mathrm{i})\;\mathrm{t}} - 1.32853 \times 10^{-15} \; \mathrm{e}^{\,(0.+6497.6\,\mathrm{i})\;\mathrm{t}} - 1.32853 \times 10^{-15} \;\mathrm{e}^{\,(0.+6497.6\,\mathrm{i})\;\mathrm{t}} - 1.32853 \mathrm{e}^{\,(0.+6497.6\,\mathrm{i})\;\mathrm{t}} - 1.32853 \mathrm{e}^{\,(0.+6497.6\,\mathrm{i})$

 $1.32853 \times 10^{-15} e^{(0.-6497.6 \, \text{i}) \, \text{t}} - 0.000020448 e^{(0.+10056.5 \, \text{i}) \, \text{t}} - 0.000020448 e^{(0.-10056.5 \, \text{i}) \, \text{t}} - 0.000020448 e$

ln[171]:= resp3 = u3[t] /. soln[[3]]

ln[172]:= resp4 = u4[t] /. soln[[4]]

 $\begin{array}{l} \text{Out} [172]= & 0.0028125 - 0.00142568 \ e^{(0.-126.173 \ i) \ t} - 0.00142568 \ e^{(0.+126.173 \ i) \ t} + \\ & 6.90236 \times 10^{-7} \ e^{(0.-553.858 \ i) \ t} + 6.90236 \times 10^{-7} \ e^{(0.+553.858 \ i) \ t} + \\ & 0.0269247 \ e^{(0.-794.983 \ i) \ t} + 0.0269247 \ e^{(0.+794.983 \ i) \ t} - 0.0276788 \ e^{(0.-805.653 \ i) \ t} - \\ & 0.0276788 \ e^{(0.+805.653 \ i) \ t} - 2.79182 \times 10^{-7} \ e^{(0.-1820.39 \ i) \ t} - 2.79182 \times 10^{-7} \ e^{(0.+1820.39 \ i) \ t} - \\ & 5.75616 \times 10^6 \ e^{(0.-2258.45 \ i) \ t} + 0.607464 \ e^{(0.+2258.45 \ i) \ t} + 5.75616 \times 10^6 \ e^{(0.-2258.45 \ i) \ t} - \\ & 0.616053 \ e^{(0.+2272.76 \ i) \ t} - 0.616053 \ e^{(0.-2272.76 \ i) \ t} + 1.5705 \times 10^{-6} \ e^{(0.-6497.6 \ i) \ t} + \\ & 1.5705 \times 10^{-6} \ e^{(0.+6497.6 \ i) \ t} + 0.0107646 \ e^{(0.-10056.5 \ i) \ t} + 0.0107646 \ e^{(0.+10056.5 \ i) \ t} \end{array}$



In[173]:= Plot[Re[resp1], {t, 0, 0.2}, PlotStyle o {Thick, Red}, PlotLabel o "Tip Response"]



In[180]:= Table[InverseLaplaceTransform[Uj[[i]], s, t], {i, 1, 4}]

Out[180]= {0.0249985, 0.00374979, 0.00781198, 0.00281232}

Problem 5

Problem Statement

Solve problem 4-4 by mode superposition. Plot the tip responses of ode45 and this solution on the same graph. Also show mode truncation effect in the modal solution. Show how it is improved by mode acceleration solutions.

Solution

A MATLAB function was developed for solving for the response of MDOF systems by mode superposition. It is available in the appendix. The plot of the tip response is shown below:



Figure 8: Tip response using mode superposition."

This result agrees well with the results obtained using the Laplace transform:



Figure 9: Tip response using the Laplace transform.

A separate MATLAB function was also developed for numerical solution of general *n*-dof systems. This was done using the following formulation:

$$\mathbf{M}\ddot{\mathbf{u}} + \mathbf{C}\dot{\mathbf{u}} + \mathbf{K}\mathbf{u} = \mathbf{F}$$
(16)

$$\frac{d\mathbf{u}}{dt} = \mathbf{v}$$
$$\frac{d^2\mathbf{u}}{dt} = \dot{\mathbf{v}}$$

Then, the system can be written as

$$\dot{\mathbf{v}} = \mathbf{A}\mathbf{v} + \mathbf{f} \tag{17}$$

where **A** is the system matrix given by

$$\mathbf{A} = \begin{bmatrix} \mathbf{0} & \mathbf{I} \\ -\mathbf{M}^{-1}\mathbf{K} & -\mathbf{M}^{-1}\mathbf{C} \end{bmatrix}$$
(18)

and **f** is given by

$$\mathbf{f} = \begin{cases} \mathbf{0} \\ \mathbf{M}^{-1} \mathbf{F} \end{cases}$$
(19)

The mode truncation solution is shown below:



Figure 10: Differences between response for different number of modes truncated.



Figure 11: Differences between response for different number of modes truncated (close-up).

The mode acceleration solutions improve the approximation as shown in the below plots, especially the close-up comparison.



Figure 12: Mode acceleration solution.



Figure 13: Comparison between mode truncation and mode acceleration methods.

Code listing

1 2

3

4 5

6

7 8

```
function [t,u] = mdof_response_num(K,M,C,F,t_final)
% This only works for step inputs, but could be generalized further
% pretty easily.
% Getting size of inputs
[n ~] = size(K);
```

```
% Initializing
9
    A = zeros(2*n);
10
    f = zeros(2*n, 1);
11
12
    % Forming A matrix
13
14
    A(1:n,n+1:2*n) = eye(n);
    Minv = inv(M);
15
    A(n+1:2*n,1:n) = -Minv*K;
16
    A(n+1:2*n,n+1:2*n) = -Minv*C;
17
18
    % Forming f
19
    f(n+1:2*n) = Minv*F;
20
21
    % Setting zero initial conditions
22
    Y0 = zeros(2*n, 1);
23
24
    % Solving ode
25
     [t,u] = ode45(@odefunc,[0 t_final],Y0);
26
27
         function dy = odefunc(t,y)
28
             dy = zeros(n, 1);
29
             dy = A*y + f;
30
         end
31
32
33
```

```
end
```

```
function [t_vec,u] = mdof_response_symb(K,M,Zeta,F,forcing_type,t_final,Omega)
1
2
    % Inputs
3
    % forcing_type = 'sine';
4
    % forcing_type = 'step';
5
6
    % Finding eigenvalues
7
    [Phi,Lambda] = eig(K,M);
8
9
    % Determining natural frequencies
10
    omega = sqrt(diag(Lambda));
11
12
    % Computing generalized matrices (proportionally damped)
13
    GM = Phi.'*M*Phi;
14
    GK = Phi.'*K*Phi;
15
    GC = zeros(size(GM));
16
    for idx = 1:numel(GM(:,1))
17
         GC(idx,idx) = 2*Zeta(idx)*omega(idx)*GM(idx);
18
     end
19
    GF = Phi.'*F;
20
21
    % Solving differential equation symbolically
22
    syms q(t) t
23
    Dq = diff(q);
24
    D2q = diff(q,2);
25
    if strcmp(forcing_type,'sine')
26
        for idx = 1:numel(GM(:,1))
27
```

```
modal_soln(idx,1) = vpa(dsolve(GM(idx,idx)*D2q + GC(idx,idx)*Dq + ...
28
                 GK(idx,idx)*q == GF(idx)*sin(Omega*t), q(0)==0,Dq(0)==0),8);
29
         end
30
     elseif strcmp(forcing_type,'step')
31
         for idx = 1:numel(GM(:,1))
32
33
             modal_soln(idx,1) = vpa(dsolve(GM(idx,idx)*D2q + GC(idx,idx)*Dq + ...
                 GK(idx,idx)*q == GF(idx), q(0)==0,Dq(0)==0),8);
34
         end
35
    end
36
37
    % Converting back to physical coordinates
38
     soln = vpa(Phi*modal_soln,8);
39
     for s = 1:numel(soln)
40
         disp(vpa(simplify(soln(s)),4));
41
    end
42
43
    % Substituting time vector
44
     t_vec = linspace(0,t_final,1000);
45
    u = zeros(numel(soln), numel(t_vec));
46
     for idx = 1:numel(soln)
47
         u(idx,:) = subs(soln(idx),t,t_vec);
48
     end
49
    % u = double(u);
50
51
52
    end
     function [f,U] = freq_resp_plots(t,u,img_path,rootname)
1
2
    xmax = 2.5e7;
3
4
    % Taking the FFT of the data
5
    f_s = 1/(t(2) - t(1));
6
    N = numel(t);
7
    n = linspace(0, N-1, N);
8
    f = n \cdot f_s/N;
9
    U = fft(u,N);
10
    if mod(N/2,2) ~= 0
11
         f = f(2:(N+1)/2);
12
         U = U(2:(N+1)/2);
13
    else
14
         f = f(2:N/2);
15
         U = U(2:N/2);
16
     end
17
    omega = 2*pi*f;
18
19
    % BODE
20
21
    figure
    subplot(2,1,1)
22
    plot(omega,abs(U),'LineWidth',1.5)
23
    xlabel('$\omega$ [rad/s]','Interpreter','LaTeX')
24
    ylabel('$|U(e^{j\omega}|$', 'Interpreter', 'LaTeX')
25
    set(gca, 'YScale', 'Log', 'XLim',[0 xmax])
26
27
    subplot(2,1,2)
```

```
plot(omega,atan2(imag(U),real(U)),'LineWidth',1.5)
28
    xlabel('$\omega$ [rad/s]','Interpreter','LaTeX')
29
    ylabel('$\phi$','Interpreter','LaTeX')
30
    set(gca,'XLim',[0 xmax])
31
    set(gcf, 'PaperPositionMode', 'Auto')
32
    print(gcf, '-depsc', [img_path, '/', rootname, '_bode'])
33
34
    % CO-QUAD
35
    figure
36
    subplot(2,1,1)
37
    plot(omega, real(U), 'LineWidth', 1.5)
38
    xlabel('$\omega$ [rad/s]','Interpreter','LaTeX')
39
    ylabel('$\Re(U)$','Interpreter','LaTeX')
40
    set(gca,'XLim',[0 xmax])
41
    subplot(2,1,2)
42
    plot(omega, imag(U), 'LineWidth', 1.5)
43
    xlabel('$\omega$ [rad/s]','Interpreter','LaTeX')
44
    ylabel('$\Im(U)$','Interpreter','LaTeX')
45
    set(gca,'XLim',[0 xmax])
46
    set(gcf,'PaperPositionMode','Auto')
47
    print(gcf, '-depsc', [img_path, '/', rootname, '_coquad'])
48
49
    % Nyquist
50
    figure
51
    plot(real(U), imag(U), 'LineWidth', 1.5);
52
    xlabel('$\Re(U)$','Interpreter','LaTeX')
53
    ylabel('$\Im(U)$','Interpreter','LaTeX')
54
    set(gcf, 'PaperPositionMode', 'Auto')
55
    print(gcf, '-depsc', [img_path, '/', rootname, '_nyquist'])
56
57
    end
58
```

```
cd %% Clearing workspace
1
2
    clc,clear,close all
3
4
    %% Calling test for part I
5
6
    hw4prob2_test
7
8
    %% Part II
9
10
    clc,clear,close all
11
12
    % Inputs from Hw3
13
    L = 25;
                         % in
14
15
    E = 1e7;
                         % psi
    rho = 0.1/386.4; % lb-s^2/in^4
16
    A = 4;
                         % in^2
17
    I = 16/12;
                        % in^4
18
    N = 6:
19
20
    a = 2;
21
```

```
% Calling beam_ritz
22
    plt_nm = '../Images/basis';
23
    [~,~,~,Ku,Mu] = beam_ritz(L,E,rho,A,I,N,'C-F','monomial','true',plt_nm);
24
    close all
25
26
    % Forming the impedance matrix
27
    syms Omega
28
    Z = Ku - Omega * Mu;
29
    H = inv(Z);
30
31
    % Enforcing |U_5| = 2 |U_3|
32
    m = 3; % the force is applied at node 3
33
    symb = abs(H(3,m)) - a*abs(H(1,m));
34
    num = matlabFunction(symb);
35
    omega_soln = fminbnd(num,0.0,1e7);
36
    fprintf('Omega = %.2f rad/s\n',omega_soln)
37
38
    Mn = subs(Mu,Omega,omega_soln);
39
    Kn = subs(Ku,Omega,omega_soln);
40
41
    [p,1] = eig(Kn,Mn);
42
43
    % Plotting
44
    Omega_v = linspace(0,3e7,50000);
45
    Obj = num(Omega_v);
46
    hold on
47
    plot(Omega_v,Obj,'LineWidth',1.5)
48
    plot(omega_soln,num(omega_soln),'ok','LineWidth',1.5,'MarkerFaceColor','g')
49
    set(gca, 'YScale', 'Log')
50
    xlabel('$\Omega$ [rad/s]','Interpreter','LaTeX')
51
    ylabel('$|H_{33}(\Omega)| - 2 |H_{13}(\Omega)|$','Interpreter','LaTeX')
52
    set(gca, 'Box', 'on')
53
    set(gcf, 'PaperPositionMode', 'Auto')
54
    print(gcf,'-depsc','../Images/hw4prob2.eps')
55
    %% Clearing workspace
1
2
    clc,clear,close all
3
    addpath(genpath(pwd))
4
5
    %% Inputs
6
7
    L = 10;
                        % in
8
    E = 1e4;
                        % psi
9
    rho = 0.1/386.4; % lb-s^2/in^4
10
    A = 4;
                        % in^2
11
                       % in^4
12
    I = 16/12;
    N = 6;
13
```

```
14 a = 2;
15 
16 % Modal damping
17 zeta1 = 0.01;
```

```
18 zeta2 = zeta1;
```

```
19
    %% Calling beam_ritz
20
21
    plt_nm = '../Images/basis';
22
     [~,~,~,Ku,Mu] = beam_ritz(L,E,rho,A,I,N,'C-F','monomial','true',plt_nm);
23
24
    close all
25
    %% Eigenvalue problem
26
27
    % Numerically evaluating
28
    Kn = double(vpa(Ku, 6));
29
    Mn = double(vpa(Mu, 6));
30
     [Phi,Lambda] = eig(Kn,Mn);
31
    omega = sqrt(diag(Lambda));
32
33
    % Forming generalized stiffness and mass matrices
34
    GM = Phi.'*Mn*Phi;
35
    GK = Phi.'*Kn*Phi;
36
37
    % Determining a0 and a1 values
38
    a0 = 2*omega(1)*omega(2)*(zeta2*omega(1) - zeta1*omega(2))/ ...
39
         (omega(1)<sup>2</sup> - omega(2)<sup>2</sup>);
40
    a1 = (2*zeta1*omega(1) - 2*zeta2*omega(2))/(omega(1)^2 - omega(2)^2);
41
42
    % Computing C matrix
43
    C = a0*Mn + a1*Kn;
44
45
    %% Using ODE45 to solve the system
46
     [t,u] = mdof_response_num(Kn,Mn,C,[1;0;0;0],2);
47
48
    %% Plotting responses
49
50
     figure
51
52
    % Tip response
53
    subplot(2,1,1);
54
     plot(t,u(:,1),'LineWidth',1.5)
55
    xlabel('t [sec]','Interpreter','LaTeX')
56
    ylabel('Tip response', 'Interpreter', 'LaTeX')
57
58
    % Mid span response
59
    subplot(2,1,2);
60
    plot(t,u(:,3),'LineWidth',1.5);
61
    xlabel('t [sec]','Interpreter','LaTeX')
62
    ylabel('Midspan response', 'Interpreter', 'LaTeX')
63
64
    % Saving figure
65
     set(gcf, 'PaperPositionMode', 'Auto')
66
    print(gcf,'-depsc','../Images/hw4prob3_responses')
67
68
    %% Computing and plotting frequency responses
69
70
    [~,~] = freq_resp_plots(t,u(:,1),'../Images','tip');
71
```

72 [~,~] = freq_resp_plots(t,u(:,3),'../Images','midspan');

```
%% Clearing workspace
1
2
    clc,clear,close all
3
    addpath(genpath(pwd))
4
5
    %% Inputs
6
7
    L = 10;
                        % in
8
    E = 1e4;
                        % psi
9
    rho = 0.1/386.4; % lb-s^2/in^4
10
    A = 4;
                        % in^2
11
    I = 16/12;
                        % in^4
12
    N = 6;
13
    a = 2;
14
15
    %% Calling beam_ritz
16
17
    plt_nm = '.../Images/basis';
18
    [~,~,~,Ku,Mu] = beam_ritz(L,E,rho,A,I,N,'C-F','monomial','true',plt_nm);
19
    close all
20
21
    K = double(vpa(Ku, 6));
22
    M = double(vpa(Mu, 6));
23
24
    %% Calling function that solves problem using mode superposition
25
26
    [t,u] = mdof_response_symb(K,M,[0;0;0;0],[1;0;0;0],'step',0.2,0);
27
28
    % Plotting results for the tip response
29
    hold on
30
    plot(t,u(1,:),'-k','LineWidth',1.5)
31
32
33
    %% Calling function that solves the problem using ODE45
34
35
    [t_n,u_n] = mdof_response_num(K,M,zeros(size(K)),[1;0;0;0],0.2);
36
37
    plot(t_n,u_n(:,1),'--r','LineWidth',1.5)
38
39
    xlabel('$t$ [sec]','Interpreter','LaTeX')
40
    ylabel('Tip response','Interpreter','LaTeX')
41
    lh = legend('Mode Superposition', 'ode45');
42
    set(lh,'Interpreter','LaTeX')
43
    set(gca, 'Box', 'on', 'YLim', [0, max(u_n(:,1))])
44
     set(gcf, 'PaperPositionMode', 'Auto')
45
    print(gcf,'-depsc','../Images/hw4prob5_modesuperposition.eps')
46
47
    %% Solving the problem using mode truncation
48
49
    [~,u3] = mode_displacement(K,M,[0;0;0;0],[1;0;0;0],'step',0.2,3,0);
50
51
    [~,u2] = mode_displacement(K,M,[0;0;0;0],[1;0;0;0],'step',0.2,2,0);
```

```
[t,u1] = mode_displacement(K,M,[0;0;0;0],[1;0;0;0],'step',0.2,1,0);
52
53
     figure('Position',[30 440 630 350])
54
     hold on
55
     plot(t_n,u_n(:,1),'-k','LineWidth',1.5)
56
     plot(t,u3(1,:),'--b','LineWidth',1.5)
57
     plot(t,u2(1,:),'--r','LineWidth',1.5)
58
     plot(t,u1(1,:),'--g','LineWidth',1.5)
59
     set(gca, 'Box', 'On')
60
     lh = legend('All modes', 'N = 3', 'N = 2', 'N = 1');
61
     set(lh,'Location','EastOutside')
62
     set(gcf, 'PaperPositionMode', 'Auto')
63
     print(gcf,'-depsc','../Images/hw4prob5_mode_trunc')
64
65
     figure('Position', [50 135 630 350])
66
67
     hold on
     plot(t_n,u_n(:,1),'-k','LineWidth',1.5)
68
     plot(t,u3(1,:),'--b','LineWidth',1.5)
69
     plot(t,u2(1,:),'--r','LineWidth',1.5)
70
     plot(t,u1(1,:),'--g','LineWidth',1.5)
71
     set(gca, 'XLim', [0.018 0.032], 'YLim', [0.0440 0.05], 'Box', 'On')
72
     lh = legend('All modes', 'N = 3', 'N = 2', 'N = 1');
73
     set(lh,'Location','EastOutside')
74
     set(gcf, 'PaperPositionMode', 'Auto')
75
     print(gcf,'-depsc','../Images/hw4prob5_mode_trunc_close')
76
77
     %% Solving the problem using mode acceleration
78
79
     [~,u3a] = mode_acceleration(K,M,[0;0;0;0],[1;0;0;0],'step',0.2,3,0);
80
     [t,u2a] = mode_acceleration(K,M,[0;0;0;0],[1;0;0;0],'step',0.2,2,0);
81
     % [t,u1] = mode_displacement(K,M,[0;0;0;0],[1;0;0;0],'step',0.2,1,0);
82
83
     figure('Position', [30 440 630 350])
84
     hold on
85
     plot(t_n,u_n(:,1),'-k','LineWidth',1.5)
86
     plot(t,u3a(1,:),'--b','LineWidth',1.5)
87
     plot(t,u2a(1,:),'--r','LineWidth',1.5)
88
     set(gca, 'Box', 'On')
89
     lh = legend('All modes', 'N = 3', 'N = 2');
90
     set(lh,'Location','EastOutside')
91
     set(gcf, 'PaperPositionMode', 'Auto')
92
     print(gcf,'-depsc','../Images/hw4prob5_mode_acc')
93
94
     % Comparing
95
     figure('Position',[30 440 630 350])
96
     hold on
97
     plot(t_n,u_n(:,1),'-k','LineWidth',1.5)
98
     plot(t,u3(1,:),'--b','LineWidth',1.5)
99
     plot(t,u2(1,:),'--r','LineWidth',1.5)
100
     plot(t,u3a(1,:),'--g','LineWidth',1.5)
101
     plot(t,u2a(1,:),'--m','LineWidth',1.5)
102
     set(gca, 'XLim', [0.018 0.032], 'YLim', [0.0440 0.05], 'Box', 'On')
103
     lh = legend('All modes', 'N = 3, truncation', 'N = 2, truncation', ...
104
         'N = 3, acceleration', 'N = 2, acceleration');
105
```

106 set(lh,'Location','EastOutside')
107 set(gcf,'PaperPositionMode','Auto')
108 print(gcf,'-depsc','../Images/hw4prob5_comparison')